

**Program:** RFEM 5, RSTAB 8, RF-FE-LTB

**Category:** Second-Order Analysis, Isotropic Linear Elasticity, Warping, Member

**Verification Example:** 0050 – Cantilever Under Torsion Without Warping

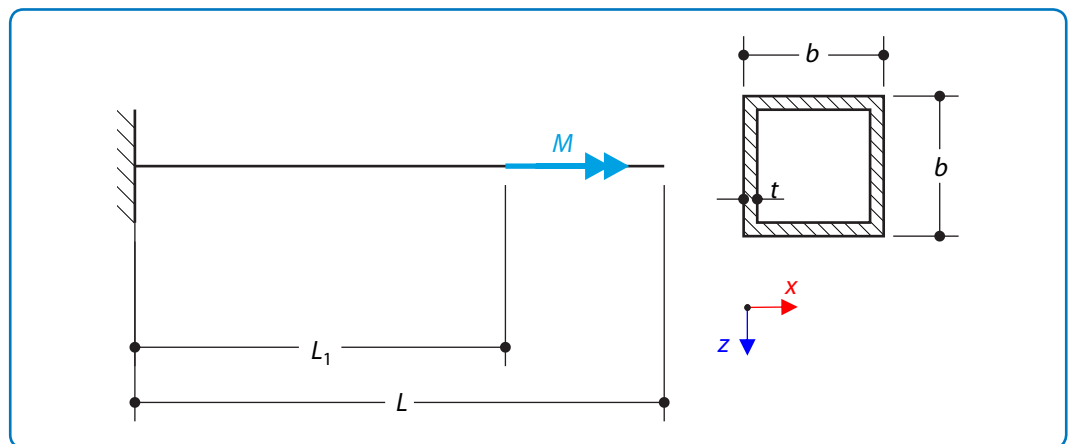
## 0050 – Cantilever Under Torsion Without Warping

### Description

A thin-walled cantilever of QRO-profile is fully fixed on the left end ( $x = 0$ ), and the warping is enabled. The cantilever is subjected to a torque  $M$  at  $x = L_1$  according to the **Figure 1** [1]. The problem is described by the following set of parameters.

Material	Steel	Modulus of Elasticity	$E$	210000.000	MPa
		Shear Modulus	$G$	81000.000	MPa
		Plastic Strength	$f_y$	355.000	MPa
Geometry	QRO Cantilever	Length	$L$	4.000	m
		Width and Height	$b$	200.000	mm
		Face Thickness	$t$	6.000	mm
Load		Torque	$M$	80.000	kNm
		Position	$L_1$	2.800	m

Small deformations are considered and the self-weight is neglected. Determine the maximum rotation  $\varphi_{x,\max}$  and control the values of the moments  $M_{T_{pri}}$ ,  $M_{T_{sec}}$  and  $M_\omega$  at the point  $x = L_1$ .



**Figure 1:** Problem sketch

### Analytical Solution

The relative twist  $\vartheta$  of the cantilever can be calculated according to the following formula

$$\vartheta = \frac{M}{GJ} = 2.252 \cdot 10^{-5} \text{ rad/mm} \quad (50 - 1)$$

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where  $J$  is the torsional constant<sup>1</sup>. For the given profile it is

$$J = 4.386 \cdot 10^7 \text{ mm}^4 \quad (50 - 2)$$

The maximum rotation about the  $x$  axis  $\varphi_{x,\max}$  occurs at the point  $x = L_1$  and it has the same value to the free end.

$$\varphi_{x,\max} = \vartheta L_1 = 0.063 \text{ rad} \quad (50 - 3)$$

For this thin-walled profile (radii in the corners are neglected) is the warping constant  $C_\omega = 0$ . Thus the moments  $M_{T\text{sec}}$  and  $M_\omega$ , which are defined below, should be zero on the full length of the profile. The primary torsional moment  $M_{T\text{pri}}$  should be coincident with the total torsional moment  $M_T$ .

$$M_\omega(x) = -EC_\omega \varphi'(x) \quad (50 - 4)$$

$$M_{T\text{sec}} = \frac{dM_\omega(x)}{dx} \quad (50 - 5)$$

### RFEM 5 and RSTAB 8 Settings

- Modeled in RFEM 5.05.0029 and RSTAB 8.05.0029
- The element size is  $l_{FE} = 0.200 \text{ m}$
- The number of increments is 5
- Isotropic linear elastic material model is used
- The structure is modeled using members

### Results

Structure Files	Program
0050.01	RFEM 5
0050.02	RSTAB 8
0050.03	RF-FE-LTB

	Analytical Solution	RFEM 5	Ratio	RSTAB 8	Ratio	RF-FE-LTB	Ratio [-]
$\varphi_{x,\max} [\text{rad}]$	0.063	0.063	1.000	0.063	1.000	0.063	1.000

In the following graphs there is demonstrated the behaviour of all the moments on the given cantilever calculated in RF-FE-LTB module. The primary torsional moment  $M_{T\text{pri}}$  should be coincident with the total torsional moment  $M_T$ . The moments  $M_{T\text{sec}}$  and  $M_\omega$  should be zero on the full length

<sup>1</sup> The torsional constant for the given profile can be approximately calculated as  $J_{\text{approx.}} = t(b-t)^3$ . The exact value is taken from RFEM 5 / RSTAB 8.

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of the profile. It can be seen there is the affected area in the nearby of the loading point ( $x = L_1$ ), when RF-FE-LTB module is used (warping is considered). Note that the above mentioned effect is getting smaller with the smoother mesh.

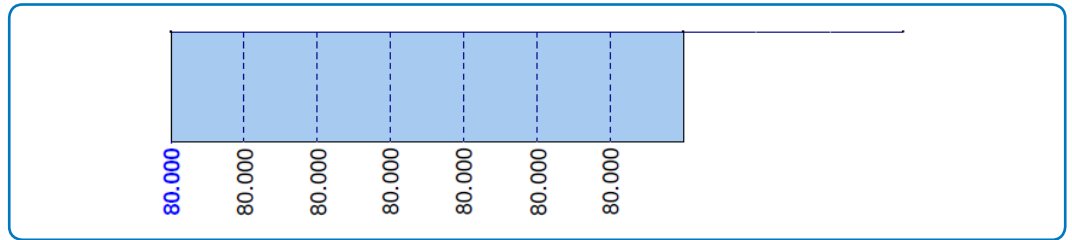


Figure 2: Total torsional moment  $M_T$  [kNm] behaviour

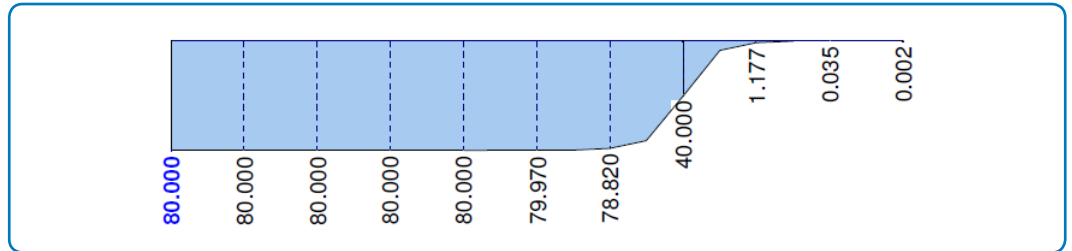


Figure 3: Primary torsional moment  $M_{T_{pri}}$  [kNm] behaviour

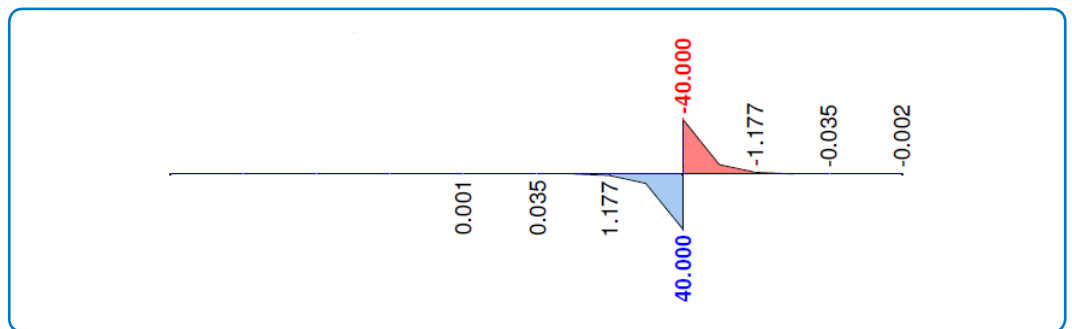


Figure 4: Secondary torsional moment  $M_{T_{sec}}$  [kNm] behaviour

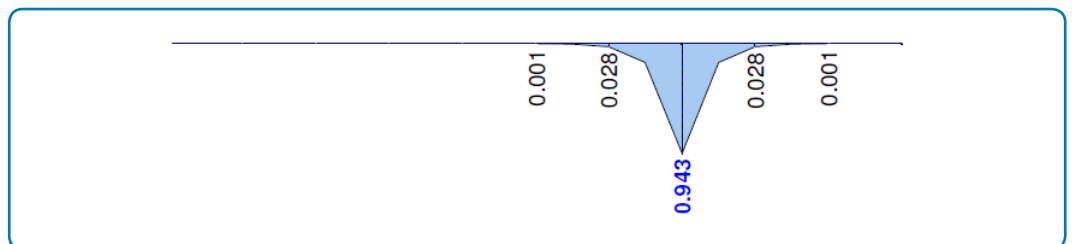


Figure 5: Warping moment  $M_w$  [kNm<sup>2</sup>] behaviour

### References

- [1] LUMPE, G. and GENSICHEN, V. *Evaluierung der linearen und nichtlinearen Stabstatik in Theorie und Software: Prüfbeispiele, Fehlerursachen, genaue Theorie*. Ernst.