

Program: RFEM 5, RF-DYNAM Pro

Category: Geometrically Linear Analysis, Isotropic Linear Elasticity, Dynamics, Plate

Verification Example: 0109 – Natural Vibrations of Circular Plate

0109 – Natural Vibrations of Circular Plate

Description

A circular steel plate of radius a and thickness h is clamped around its circumference $r = a$ according to **Figure 1**. Determine the natural frequencies of the circular plate. The problem is described by the following parameters.

Material	Steel	Modulus of Elasticity	E	210000.0	MPa
		Poisson's Ratio	ν	0.300	–
		Density	ρ	7850.000	kgm ⁻³
Geometry		Radius	a	0.500	m
		Thickness	h	0.001	m

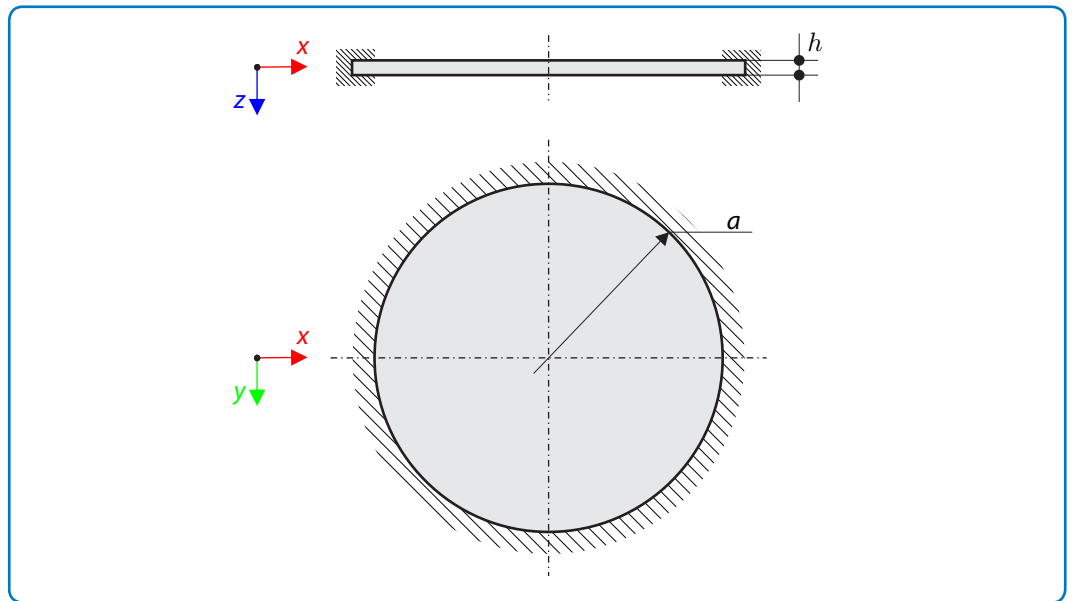


Figure 1: Problem Sketch

Analytical Solution

Free vibrations of a circular plate can be described by the wave equation in polar coordinates r, φ

$$\left(\frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \varphi^2} \right)^2 u_z + \frac{1}{c^2} \frac{\partial^2}{\partial t^2} u_z = 0 \quad (109 - 1)$$

where $u_z = u_z(r, \varphi, t)$ is the deflection in transversal direction. The speed of the wave propagation c is given by the density of the plate density ρ , plate thickness h and the plate modulus D

Verification Example: 0109 – Natural Vibrations of Circular Plate

$$c = \sqrt{\frac{D}{\rho h}}, \quad D = \frac{Eh^3}{12(1-\nu^2)} \quad (109-2)$$

The solution is sought for in following form

$$u_z(r, \varphi, t) = W(r, \varphi)e^{i\Omega t} \quad (109-3)$$

After substitution into (109 – 1), the following equation is obtained

$$\Delta^2 W - \frac{\Omega^2}{c^2} W = 0 \quad (109-4)$$

where Δ is the Laplace operator in polar coordinates, more precisely

$$\Delta = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \varphi^2} \quad (109-5)$$

hence, (109 – 4) can be rewritten as

$$\left(\Delta + \frac{\Omega}{c}\right) \left(\Delta - \frac{\Omega}{c}\right) W = 0 \quad (109-6)$$

Thus two independent equations have to be solved further

$$\left(\Delta + \frac{\Omega}{c}\right) = 0, \quad \left(\Delta - \frac{\Omega}{c}\right) = 0 \quad (109-7)$$

Assuming that the variables of $W(r, \varphi)$ are separated, i.e., $W = R(r)F(\varphi)$, (109 – 7) yields¹

$$r^2 \frac{R''}{R} + r \frac{R'}{R} \pm r^2 \frac{\Omega}{c} = m^2 = -\frac{F''}{F} \quad (109-8)$$

The left-hand side of the equation depends on the radius r , and the right-hand side depends on the angle φ , which are independent variables. Thus, both sides have to be equal to a constant m^2 .

The angle-dependent equation $F'' + m^2 F = 0$ admits the solution

$$F(\varphi) = A \sin(m\varphi) + B \cos(m\varphi) \quad (109-9)$$

where the constants A, B are defined by the boundary conditions.

On the other hand, the radius-dependent equations can be rewritten into the Bessel and modified Bessel differential equations, more precisely

¹ The dashed notation indicates the derivative with respect to the appropriate spatial coordinate, e.g., $R'' = \frac{d^2 R}{dr^2}(r)$.

Verification Example: 0109 – Natural Vibrations of Circular Plate

$$r^2 R'' + rR' \pm \left(r^2 \frac{\Omega}{c} - m^2 \right) R = 0 \quad (109 - 10)$$

The solution of the Bessel equations take the form

$$R(r) = CJ_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right) + DY_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right), \quad n = 1, 2, 3, \dots \quad (109 - 11)$$

$$R(r) = EI_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right) + FK_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right), \quad n = 1, 2, 3, \dots \quad (109 - 12)$$

where J_m and Y_m are Bessel functions and I_m and K_m are modified Bessel functions.

For the circular plate, Bessel functions Y_m and K_m become unbounded as $r \rightarrow 0$, therefore the constants D, F have to equal zero. The general solution is then rewritten in the form of linear combination with constants C_1, C_2 as

$$R(r) = C_1 J_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right) + C_2 I_m \left(\sqrt{\frac{\Omega_{mn}}{c}} r \right) \quad (109 - 13)$$

For the clamped plate, the following boundary conditions are prescribed

$$R(a) = C_1 J_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) + C_2 I_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) = 0 \quad (109 - 14)$$

$$R'(a) = C_1 J'_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) + C_2 I'_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) = 0 \quad (109 - 15)$$

where the dash denotes the derivative of the appropriate Bessel function. These derivatives can be replaced according to general formulas for Bessel functions

$$J'_m(x) = -J_{m+1}(x) + \frac{mJ_m(x)}{x} \quad (109 - 16)$$

$$I'_m(x) = I_{m+1}(x) + \frac{mI_m(x)}{x} \quad (109 - 17)$$

$$I_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) J_{m+1} \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) + J_m \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) I_{m+1} \left(\sqrt{\frac{\Omega_{mn}}{c}} a \right) = 0 \quad (109 - 18)$$

From the roots of this equation the set of constants Ω_{mn} is obtained. Considering $\Omega_{mn} = 2\pi f_{mn}$, the set of natural frequencies f_{mn} of the clamped circular plate can be calculated. The first six natural frequencies can be found in the result table.

RFEM 5 Settings

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- Modeled in RFEM 5.07.05
- The element size is $l_{FE} = 0.010$ m
- For entity type Solid, layered mesh is used with 4 layers
- Isotropic linear elastic material model is used

Results

Structure Files	Program	Entity
0109.01	RF-DYNAM Pro	Plate
0109.02	RF-DYNAM Pro	Solid

Frequency	Analytical Solution	Plate		Solid	
		RF-DYNAM Pro	Ratio	RF-DYNAM Pro	Ratio
f_1 [Hz]	10.179	10.179	1.000	10.253	1.007
f_2 [Hz]	21.184	21.184	1.000	21.343	1.008
f_3 [Hz]	34.752	34.751	1.000	35.020	1.008
f_4 [Hz]	39.629	39.624	1.000	39.940	1.008
f_5 [Hz]	50.847	50.844	1.000	51.251	1.008
f_6 [Hz]	60.611	60.604	1.000	61.118	1.008

Following **Figure 2** shows the first six natural shapes of the investigated plate.

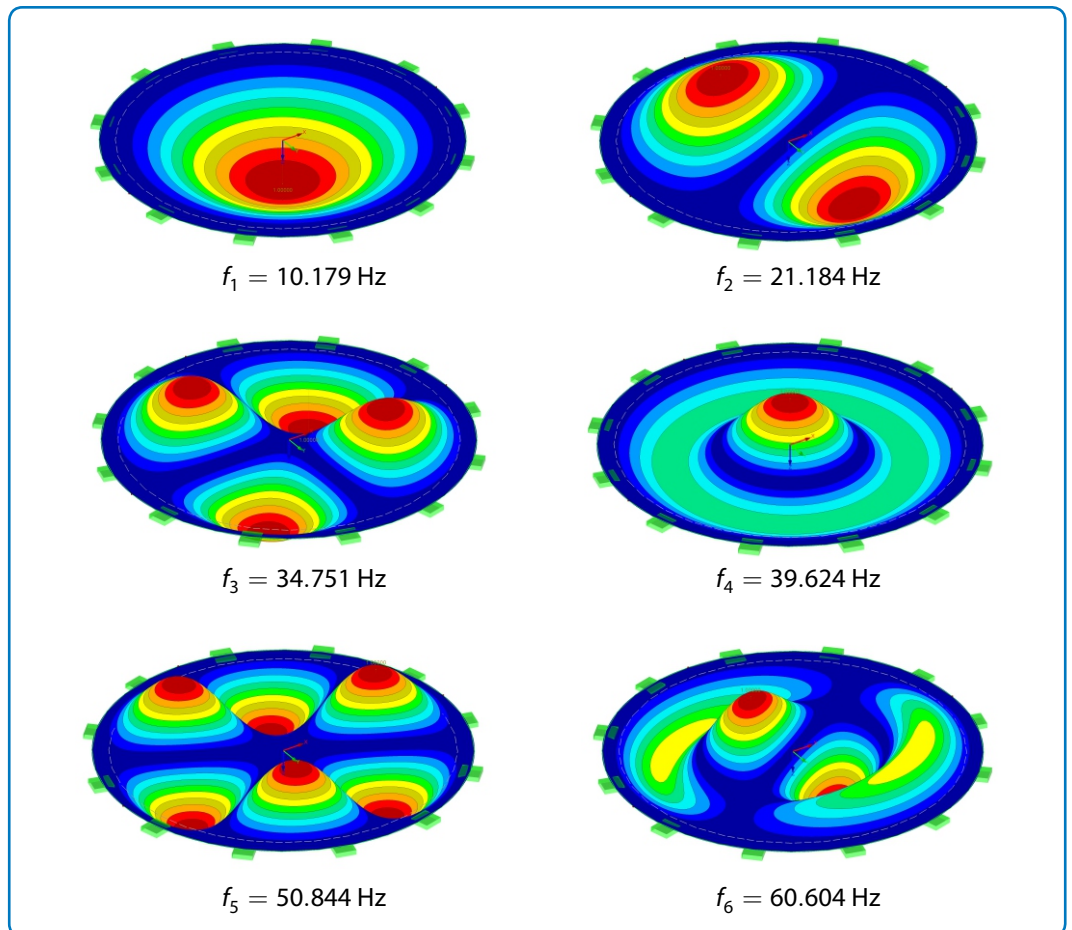


Figure 2: First six natural shapes of the plate in RFEM 5