## Category: Geometrically Linear Analysis, Isotropic Linear Elasticity, Member, Solid

## Verification Example: 0075 - Combined Loading - Reduced Stress

## 0075 - Combined Loading - Reduced Stress

## Description

A cantilever with circular cross-section is loaded by a concentrated bending force and torque. The aim of this verification example is to compare the reduced stress according to the von Mises and Tresca theories.

| Material | Modulus of <br> Elasticity | $E$ | 210000.000 | MPa |
| :--- | :--- | :--- | :--- | ---: |
|  | Poisson's Ratio | $\nu$ | 0.296 | - |
| Geometry | Diameter | $d$ | 50.000 | mm |
|  | Length | $L$ | 1000.000 | mm |
| Load | Bending Force | $F$ | 1000.000 | N |
|  | Torque | $M$ | $1.000 \times 10^{6}$ | Nmm |



Figure 1: Problem Sketch
While neglecting self-weight, determine the reduced stress according to the von Mises and Tresca theory $\sigma_{\text {Mises }}(L / 2), \sigma_{\text {Tresca }}(L / 2)$ at the mid-point of the cantilever.

## Analytical Solution

The resultant total stress at the mid-point of the cantilever is decomposed into three components, namely the bending and shear stresses $\sigma_{b}, \tau_{z}$ due to the concentrated force $F$, and the shear stress $\tau$ due to the torque $M$.

$$
\begin{equation*}
\sigma_{\mathrm{b}}(L / 2)=\frac{F L}{2 S_{y}}, \quad \tau_{z}(L / 2)=\frac{F}{A}, \quad \tau(L / 2)=\frac{M}{S_{t}} \tag{75-1}
\end{equation*}
$$

where $S_{y}$ and $S_{t}$ are the elastic and torsional section moduli of the cross-section, and $A$ is the area of the cross-section

$$
\begin{equation*}
S_{y}=\frac{\pi d^{3}}{32}, \quad S_{t}=\frac{\pi d^{3}}{16}, \quad A=\frac{\pi d^{2}}{4} \tag{75-2}
\end{equation*}
$$

## Verification Example: 0075 - Combined Loading - Reduced Stress

Taking into account all above mentioned stress components, the reduced stress is computed according to the von Mises and Tresca theories

$$
\begin{equation*}
\sigma_{\text {Mises }}(L / 2)=\sqrt{\sigma^{2}+3\left(\tau+\tau_{z}\right)^{2}} \approx 82.252 \mathrm{MPa} \tag{75-3}
\end{equation*}
$$

$$
\begin{equation*}
\sigma_{\text {Tresca }}(L / 2)=\sqrt{\sigma^{2}+4\left(\tau+\tau_{z}\right)^{2}} \approx 92.018 \mathrm{MPa} \tag{75-4}
\end{equation*}
$$

## RFEM 5 Settings

- Modeled in RFEM 5.07.05
- The element size is $I_{\text {FE }}=0.005 \mathrm{~m}$
- The number of increments is 10
- Isotropic linear elastic model is used
- Shear stiffness of members is activated


## Results

| Structure Files | Entity |
| :---: | :---: |
| 0075.01 | Member |
| 0075.02 | Solid |


| Quantity <br> $[M P a]$ | Analytical <br> Solution | RFEM 5 <br> Member | Ratio | RFEM 5 <br> Solid | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\sigma_{\text {Mises }}(L / 2)$ | 82.252 | 81.693 | 0.993 | 82.554 | 1.004 |
| $\sigma_{\text {Tresca }}(L / 2)$ | 92.018 | 91.344 | 0.993 | 92.273 | 1.003 |

Remark
When using member entity, the cantilever is modeled at half the length to obtain results equivalent to the solid model. For member models, the results are read in the fixed node. For solid models, the results are read from the section in the half of the cantilever.

