## Program: RFEM 5

## Category: Geometrically Linear Analysis, Orthotropic Plasticity, Plate, Solid

## Verification Example: 0010 - One-dimensional Orthotropic Plasticity - 4 Columns

## 0010 - One-dimensional Orthotropic Plasticity - 4 Columns

## Description

Four columns with width $d$, depth $d$, height $h$ and distance $d$ between them are oriented in the direction of the $Z$-axis. They are fixed at the bottom and connected by the rigid block at the top. Block is loaded by the pressure $p$ in the $Z$-direction and modeled by an elastic material with high modulus of elasticity $E_{\mathrm{r}}$. Outer columns are modeled as orthotropic elastic material and inner columns as orthotropic elastic-plastic material with the same elastic parameters as outer columns and with plasticity properties defined according to the Tsai-Wu plasticity theory. Material fibers are oriented by angles $-45^{\circ}$ and $45^{\circ}$ (Figure 1). Assuming only small deformations theory and neglecting structure's self-weight, determine its maximum deflection.

| Material | Columns | Modulus of | $E_{x}=E_{y}$ | 3000.000 | MPa |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Elasticity | $E_{z}$ | 11000.000 | MPa |
|  |  | Poisson's Ratio | $\nu_{x y}=\nu_{x z}=\nu_{y z}$ | 0.000 | - |
|  |  | Shear <br> Modulus | $G_{x y}=G_{x z}=G_{y z}$ | 5500.000 | MPa |
|  | Inner Columns Plasticity | Tensile Plastic Strength | $f_{\mathrm{t}, x}=f_{\mathrm{t}, z}$ | 3.000 | MPa |
|  |  |  | $f_{t, y}$ | 2.121 | MPa |
|  |  | Compressive <br> Plastic <br> Strength | $f_{c, \chi}=f_{c, z}$ | 3.000 | MPa |
|  |  |  | $f_{c, y}$ | 2.121 | MPa |
|  |  | Shear Tensile <br> Plastic <br> Strength | $f_{v, x y}=f_{v, x z}=f_{v, y z}$ | 99999.000 | MPa |
|  | Block | Modulus of Elasticity | $E_{r}$ | 20000000.000 | MPa |
|  |  | Poisson's <br> Ratio | $\nu_{\mathrm{r}}$ | 0.000 | - |
| Geometry | Column | Height | $h$ | 1.000 | m |
|  |  | Depth <br> Width <br> Distance | $d$ | 0.050 | m |
|  | Block | Height | d | 0.050 | m |
|  |  | Width | 7d | 0.350 | m |
| Load |  | Pressure | $p$ | 4.571 | MPa |

Verification Example: 0010-One-dimensional Orthotropic Plasticity - 4 Columns


Figure 1: Problem sketch

## Analytical Solution

## Linear Analysis

Formula for the maximum displacement can be evaluated with the use of the transformed stiffness matrix into the loading direction (see verification example 0007 for the detailed description):

$$
\begin{equation*}
u_{\max }=\sigma_{L} h\left(\frac{\sin ^{4} \beta}{E_{x}}+\frac{\cos ^{4} \beta}{E_{z}}+\frac{\sin ^{2} \beta \cos ^{2} \beta}{G_{x z}}\right) \tag{10-1}
\end{equation*}
$$

where $\sigma_{L}$ is the loading pressure per one column:

$$
\begin{equation*}
\sigma_{L}=\frac{7 p d^{2}}{4 d^{2}}=\frac{7}{4} p \tag{10-2}
\end{equation*}
$$

## Nonlinear Analysis

The maximum deformation of the structure can be obtained by:

$$
\begin{equation*}
u_{\max }=h \varepsilon=h \frac{\sigma_{\mathrm{el}}}{E_{\mathrm{eff}}} \tag{10-3}
\end{equation*}
$$

where $E_{\text {eff }}$ is the corresponding effective modulus of elasticity in the Z-direction:

$$
\begin{equation*}
E_{\mathrm{eff}}=\frac{\sigma_{L}}{u_{Z, \max }} \tag{10-4}
\end{equation*}
$$

where $u_{Z, \text { max }}$ is the elastic deformation of one column in the $Z$-direction and can be described same as in (10-1):

$$
\begin{equation*}
u_{z, \max }=\sigma_{\mathrm{el}} h\left(\frac{\sin ^{4} \beta}{E_{x}}+\frac{\cos ^{4} \beta}{E_{z}}+\frac{\sin ^{2} \beta \cos ^{2} \beta}{G_{x z}}\right) \tag{10-5}
\end{equation*}
$$

where $\sigma_{\text {el }}$ is the stress in the elastic column:

$$
\begin{equation*}
\sigma_{\mathrm{el}}=2 \sigma_{\mathrm{L}}-\sigma_{Z, \mathrm{el}} \tag{10-6}
\end{equation*}
$$

where $\sigma_{Z, \text { el }}$ is the stress in the plastic column, which under these circumstances can be expressed according to the Tsai-Wu surface condition as follows (see verification example 0009 for the detailed description):

$$
\begin{equation*}
\sigma_{z, \mathrm{el}}=\sqrt{2 f_{\mathrm{t}, \mathrm{z}} f_{\mathrm{c}, \mathrm{z}}} \tag{10-7}
\end{equation*}
$$

Substituting those formulae into the equation (10-3), the maximum deformation can be obtained:

$$
u_{\max }=h^{2}\left(\frac{\sin ^{4} \beta}{E_{x}}+\frac{\cos ^{4} \beta}{E_{z}}+\frac{\sin ^{2} \beta \cos ^{2} \beta}{G_{x z}}\right)\left(\frac{7}{2} p-\sqrt{2 f_{\mathrm{t}, \mathrm{z}} f_{c, z}}\right)=1.781 \mathrm{~mm} \quad(10-8)
$$

## RFEM 5 Settings

- Modeled in version RFEM 5.03.0050
- The element size is $I_{\mathrm{FE}}=0.025 \mathrm{~m}$
- Geometrically linear analysis is considered
- The number of increments is 5


## Results

| Structure File | Entity | Material Model |
| :---: | :---: | :---: |
| 0010.01 | Solid | Orthotropic Plastic 3D |
| 0010.02 | Plate | Orthotropic Plastic 2D |
| 0010.03 | Solid | Orthotropic Elastic 3D |
| 0010.04 | Plate | Orthotropic Elastic 2D |



Figure 2: Model and results in RFEM 5
As can be seen from the following comparisons, good agreements of analytical result and outputs from RFEM were achieved.

Linear Analysis

| Analytical <br> Solution | RFEM 5 <br> Orthotropic Elastic 3D |  | RFEM 5 <br> Orthotropic Elastic 2D |  |
| :---: | :---: | :---: | :---: | :---: |
| $u_{\max }$ <br> $[\mathrm{mm}]$ | $u_{\max }$ <br> $[\mathrm{mm}]$ | Ratio <br> $[-]$ | $u_{\max }$ <br> $[\mathrm{mm}]$ | Ratio <br> $[-]$ |
| 1.212 | 1.206 | 0.995 | 1.206 | 0.995 |

Nonlinear Analysis

| Analytical <br> Solution | RFEM 5 |  | RFEM 5 |  |
| :---: | :---: | :---: | :---: | :---: |
| $u_{\max }$ <br> $[\mathrm{mm}]$ | $u_{\max }$ <br> $[\mathrm{mm}]$ | Ratio <br> $[-]$ | $u_{\max }$ <br> $[\mathrm{mm}]$ | Ratio <br> $[-]$ |
| 1.781 | 1.772 | 0.995 | 1.773 | 0.996 |

